



Optimization Study of Blended Nanoparticles – Palm Biodiesel Fuel on The Performance of Marine Diesel Engine

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ABSTRACT

The marine shipping industry's significant contribution to global emissions has intensified the search for cleaner fuel alternatives. This study investigated the optimization of nanoparticle-blended palm biodiesel fuel for marine diesel engine applications, focusing on both performance enhancement and emissions reduction. Three types of metal oxide nanoparticles (SiO_2 , Al_2O_3 , and TiO_2) were evaluated at concentrations of 50, 100, and 150 ppm in a B20 palm biodiesel blend. Initial stability tests over a 15-day period revealed that only SiO_2 -blended samples maintained the required stability for engine testing. Experimental investigations were conducted on a Cummins NT-855 marine diesel engine coupled with a 250-kW dynamometer, operating at a constant speed of 1400 rpm under varying load conditions. Response Surface Methodology (RSM) with Central Composite Design (CCD) was employed to optimize the relationship between input variables (engine load and nanoparticle concentration) and response parameters (brake torque, brake power, and emissions). The study revealed that SiO_2 nanoparticles at 67.26 ppm concentration under 200 Nm engine load provided optimal performance, achieving 95.3% desirability with significant reductions in CO, CO_2 , and NOx emissions. Statistical analysis through ANOVA validated the model's accuracy with an R^2 value exceeding 0.95. This research demonstrates the potential of nanoparticle-enhanced biodiesel as a viable solution for reducing marine engine emissions while maintaining performance standards.

1. Introduction

International shipping transportation plays a pivotal role in the global economy, with the sector responsible for transporting approximately 90% of global trade [1-3]. This extensive maritime activity, however, comes with significant environmental implications. In 2015, the global shipping fleet consumed approximately 298 million tonnes of fuel, resulting in substantial emissions of CO_2 , greenhouse gases (GHG), sulphur oxides (SOx), nitrogen oxides (NOx), and particulate matter [4]. The International Maritime Organization's (IMO) implementation of a global 0.5% sulphur content limit on marine fuels in January 2020 has compelled the shipping industry to explore alternative marine

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bunker fuels with improved environmental performance. The environmental impact of combustion-related emissions, including nitrogen oxides (NO_x), carbon monoxide (CO), total unburned hydrocarbons (HC), soot, and greenhouse gases, has become increasingly concerning. Additionally, the reliance on petroleum-based fuels, being non-renewable resources, poses potential energy security risks for future generations [5,6]. These challenges have intensified the search for sustainable alternative fuel solutions in the maritime sector. Among various alternatives, biodiesel has emerged as a promising candidate due to its comparable fuel characteristics to conventional diesel and its potential for reduced environmental impact [7,8].

Palm biodiesel, in particular, has gained significant attention due to its favourable properties and widespread availability. Recent studies have demonstrated that palm oil-based biodiesel offers several advantages, including high cetane number, good oxidation stability, and reduced emissions compared to conventional diesel [9]. However, certain limitations such as higher viscosity and lower energy content have prompted researchers to investigate enhancement strategies. One particularly promising approach involves the integration of nanoparticles as fuel additives [10,11]. The addition of nanoparticles to biodiesel has shown remarkable potential in improving fuel performance while simultaneously reducing exhaust emissions. Recent research has demonstrated that various types of nanoparticles, including metal oxides (Al₂O₃, TiO₂) and carbon-based materials (CNTs, graphene oxide), can significantly enhance combustion characteristics and engine performance [12-14]. These improvements include increased brake thermal efficiency, reduced specific fuel consumption, and lower emissions of NO_x and particulate matter.

Response Surface Methodology (RSM) has emerged as a powerful statistical tool for optimizing complex processes in engine research. Several studies have demonstrated its effectiveness in biodiesel optimization. Uslu *et al.*, employed RSM to optimize nanoparticle concentrations in biodiesel blends, achieving an overall high desirability value of 0.7665 [15]. Similarly, Khan *et al.*, utilized RSM to optimize the engine performance parameters and found RSM is an efficient and effective optimization technique for gasoline engines operating within multi-objective optimization configurations [16]. The Box-Behnken design, a specific RSM approach, has proven particularly effective for fuel optimization studies. The advantage of RSM lies in its ability to generate mathematical models that accurately predict system behaviour while minimizing the number of required experiments. Recent studies have demonstrated its effectiveness in handling multiple response variables simultaneously. Singh *et al.*, used RSM to optimize ZnO nanoparticle concentrations in ternary biodiesel blends, resulting in improved engine performance and reduced emissions [17].

Despite these advancements, significant research gaps remain in understanding the complex interactions between nanoparticle-enhanced palm biodiesel and marine diesel engine performance, particularly in the context of optimization using RSM. Therefore, this study aims to investigate the effects of different nanoparticle concentrations on palm biodiesel fuel properties, optimize the blending parameters using Response Surface Methodology, evaluate emission characteristics under various engine operating conditions, and develop predictive models for engine performance and emissions using RSM to facilitate future optimization efforts.

2. Methodology

2.1 Fuel Preparation

Commercial-grade diesel fuel (B0) and palm-derived biodiesel (B100) meeting EN 14214 standards were obtained from a certified local supplier. The B20 blend was prepared by mixing 80% diesel and 20% biodiesel by volume using a calibrated mechanical stirrer operating at 1000 rpm for

30 minutes at room temperature ($25 \pm 2^\circ\text{C}$). The base fuel properties were verified through laboratory testing according to ASTM standards to ensure consistency throughout the experiments. Three types of metal oxide nanoparticles were selected: silicon dioxide (SiO_2 , 50 nm), aluminium oxide (Al_2O_3 , 40 nm), and titanium dioxide (TiO_2 , 30 nm), each with purity exceeding 99.5%.

Nine distinct fuel samples were prepared by blending B20 with each type of nanoparticle at concentrations of 50, 100, and 150 ppm. The blending process parameters were established based on previous successful studies in nanoparticle-fuel preparation. The ultrasonication frequency of 30 kHz for 30 minutes was adopted following the optimal parameters identified by Gavhane *et al.*, who demonstrated that this frequency provided effective nanoparticle dispersion while preventing particle agglomeration [18]. The magnetic stirring speed of 2400 rpm for 30 minutes was based on the work of Mostafa *et al.*, who found this combination optimal for achieving uniform nanoparticle distribution in diesel blends [19]. The stability evaluation period of 15 days was maintained under a controlled temperature of $25 \pm 2^\circ\text{C}$ and relative humidity of $60 \pm 5\%$, following the protocols established by previous researchers for nanoparticle-enhanced fuel stability studies [12,20,21]. Visual inspections revealed that only SiO_2 -blended samples maintained stability without sedimentation, while TiO_2 and Al_2O_3 blends showed significant sedimentation, making them unsuitable for engine testing due to potential injection system damage. Consequently, only the SiO_2 nanoparticle-blended samples were selected for subsequent engine performance testing.

2.2 Engine Testing

The experimental investigations were conducted on a Cummins NT855 marine diesel engine, a 4-stroke inline 6-cylinder configuration specifically designed for marine applications. The engine was coupled to a SAJ SE-250 eddy-current dynamometer with a maximum power absorption capacity of 250 kW. Engine control and data acquisition were managed through an integrated digital control system. The complete engine specifications are presented in Table 1.

The test setup incorporated comprehensive instrumentation for performance and emissions analysis (Figure 1). Torque measurements were conducted using a high-precision load cell integrated with the dynamometer, while engine speed was monitored via a digital tachometer with ± 1 rpm accuracy. The engine loading was precisely controlled through the SE-250 dynamometer controller by modulating the electromagnetic field strength. Tests were performed at five discrete load points (0, 50, 100, 150, and 200 Nm) while maintaining a constant engine speed of 1400 ± 5 rpm. Exhaust gas emissions were continuously monitored using a calibrated TAYLOR gas analyser capable of measuring CO, CO_2 , HC, NO_x, and O_2 concentrations. All measurements were recorded after achieving steady-state conditions, defined as parameter variations within $\pm 2\%$ over a 3-minute period.

Table 1
Engine specifications

Specification	Description
Engine type	4-cycle, Inline, 6-cylinder
Bore and Stroke	139 mm x 152 mm
Displacement volume	14 liters
Compression ratio	14.5
Maximum torque	1068 Nm
Maximum power	201 kW
Cooling system	Water cooling

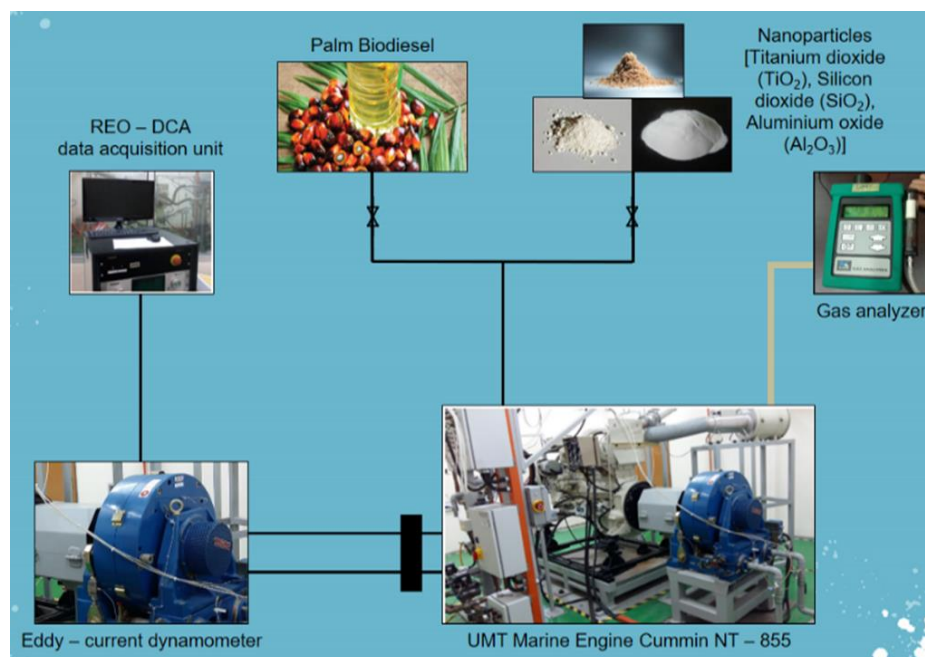


Fig. 1. Schematic diagram of the experimental setup

2.3 Design of Experiment

The experimental investigation utilized Response Surface Methodology (RSM) through Design Expert Software to optimize engine performance and emission parameters. A Central Composite Design (CCD) was implemented to establish the relationship between input variables and response parameters. Two independent variables were considered: engine load (X_1 : 100-200 Nm) and SiO_2 nanoparticle concentration (X_2 : 50-150 ppm). The response variables encompassed both performance parameters (brake torque and brake power) and emission characteristics (CO , CO_2 , and NO_x emissions) as listed in Table 2. The experimental design comprised 13 runs, including centre points to ensure statistical validity. The mathematical relationship between the response variables (Y) and independent variables was modelled using a second-order polynomial equation:

$$y = b_0 + b_1x_1 + b_2x_2 + b_{11}x_1^2 + b_{22}x_2^2 + b_{12}x_1x_2 \quad (1)$$

Where X_1 represents the engine load and X_2 represents the nanoparticle concentration. The statistical significance of the developed models was evaluated through analysis of variance (ANOVA), and the adequacy of the models was verified using various statistical criteria including R^2 , adjusted R^2 , predicted R^2 , and lack of fit tests. Three-dimensional response surface plots and contour plots were generated to visualize the interactive effects of the independent variables on the response parameters and to identify optimal operating conditions.

Table 2

Experimental design matrix

Std. run	A: Engine load (Nm)	B: SiO_2 concentration (ppm)	Brake torque (Nm)	Brake power (kW)	CO (vol%)	CO_2 (vol%)	NO_x (ppm)
11	150	100	15.6	22.4	0.26	45.1	1515
2	200	50	20	28.7	0.35	142.9	793
9	150	100	15.4	22.1	0.26	45.5	1515
7	150	50	15.5	22.2	0.35	129.9	1654
13	150	100	20.4	29.3	0.29	52.1	1668

12	150	100	15.4	22.1	0.26	46.1	1537
1	100	50	10.3	14.7	0.31	90.8	1648
8	150	150	15.6	22.4	0.32	58.6	1514
4	200	150	20.4	29.3	0.32	86.8	1648
5	100	100	15.4	22.1	0.26	45.6	1537
10	150	100	15.4	22.2	0.26	45.2	1537
3	100	150	10.2	14.6	0.28	31.2	1141
6	200	100	20.4	29.3	0.29	52.1	1668

3. Results and Discussion

3.1 Fuel Properties

The primary fuel properties of B0 (pure diesel), B20 (biodiesel blend), B100 (pure biodiesel), and the fuel blends with nanoparticles were evaluated, as summarized in Tables 3 and 4.

Table 3

Properties of B0, B20, and B100 fuels

Property	Method	Units	B0	B20	B100
Kinematic viscosity (40°C)	ASTM D7042	mm ² /s	3.4725	3.4737	3.9160
Density (15°C)	ASTM D7042	kg/m ³	811.89	815.62	834.91
Heating value	ASTM D240	J/g	45886	44747	42130

Table 4

Comparison of thermo-physical properties of fuel blends

Fuel Blend	ppm	Kinematic viscosity (mm ² /s)	Density (kg/m ³)	Heating value (J/g)
B20 + SiO ₂	50	3.5916	817.74	45090
B20 + SiO ₂	150	3.7792	820.36	45122
B20 + Al ₂ O ₃	50	3.6224	818.28	44958
B20 + TiO ₂	150	3.6019	817.96	45110

The evaluation of fuel properties revealed significant improvements in the blends with nanoparticle additives. The B20 blend with SiO₂ nanoparticles exhibited enhanced density and heating values compared to the base biodiesel. Specifically, the B20 + SiO₂ (150 ppm) blend showed a notable increase in kinematic viscosity and density, leading to better fuel performance. However, it was observed that the blends with TiO₂ and Al₂O₃ nanoparticles experienced sedimentation issues, which could affect the stability and performance of the fuel. Consequently, these blends were deemed unsuitable for further engine testing due to potential operational concerns.

3.2 Analysis of Variance (ANOVA)

The ANOVA results provide insights into the statistical significance of the regression models developed for engine performance and emissions. Table 5 summarizes the results of the Analysis of Variance (ANOVA) conducted for the experiments, along with the numerical data concerning the p-values. The probability value (p-value) serves as a criterion for determining the minimum significance level at which the null hypothesis can be rejected. According to the ANOVA results, all models have a p-value of less than 0.05, indicating statistical significance. Additionally, Table 5 displays the regression model coefficients, R² values, and p-values for each dependent variable. The findings reveal that the proposed models are suitable, with minimal deviations and acceptable R² values for all independent variables (responses). By comparing the predicted data from the models with the

experimental data, the validation process confirms that the models fit well and the variables are highly correlated.

Table 5

Analysis of variance (ANOVA)

Source	Brake Power	p-value	Brake Torque	p-value	CO emission	p-value	CO ₂ emission	p-value	NO _x emission	p-value
A- Engine Load	26.81	0.0004	26.81	0.0004	10.59	0.0140	17.06	0.0044	0.2546	0.6260
B- Concentration of SiO ₂	0.0102	0.9216	0.0069	0.9354	7.09	0.0324	45.75	0.0003	0.2339	0.6402
AB	-	-	-	-	9.107E-15	1.0000	0.0240	0.8812	15.04	0.0037
A ²	-	-	-	-	0.3625	0.5661	0.0861	0.7777	-	-
B ²	-	-	-	-	43.86	0.0003	40.85	0.0004	-	-
R ²	0.7284		0.7283		0.9039		0.9397		0.6331	

3.3 Engine Performance Model

3.3.1 Brake torque

The interaction effect of nanoparticle concentration in B20 blended with SiO₂ and engine speed on brake torque is illustrated in Figures 2 and 3. The contour surface plot in these figures shows that the addition of SiO₂ in B20 fuel increases brake torque across all engine speeds. As both the concentration of nanoparticles in the fuel and engine speed increase, the brake torque also increases. The graph demonstrates a clear trend where higher concentrations of SiO₂ nanoparticles combined with increased engine speeds result in enhanced brake torque. This indicates that SiO₂ acts as an effective additive in improving engine performance.

This relationship is represented by the regression model obtained using Design Expert Software, as shown in Eq. (2).

$$\text{Brake Torque} = 16.15 + 4.15A + 0.0667B \quad (2)$$

3.3.2 Brake power

Figures 4 and 5 present the predicted values of brake power for B20 blended with SiO₂ at various engine speeds. The contour surface plot reveals that increasing the nanoparticle content in the B20 fuel leads to a slight increase in engine brake power across all engine speeds, suggesting optimized combustion. The data clearly show that both engine speed and nanoparticle concentration in B20 fuel significantly affect brake power, as described by the regression model in Eq. (3).

$$\text{Brake Power} = 23.18 + 5.98A + 0.1167B \quad (3)$$

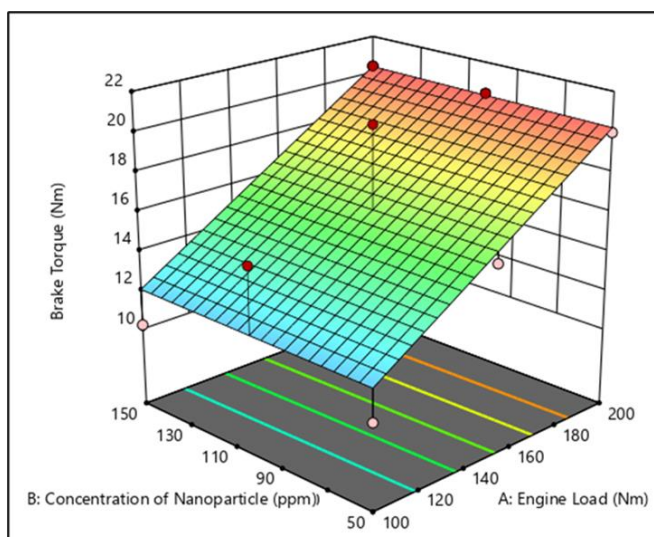
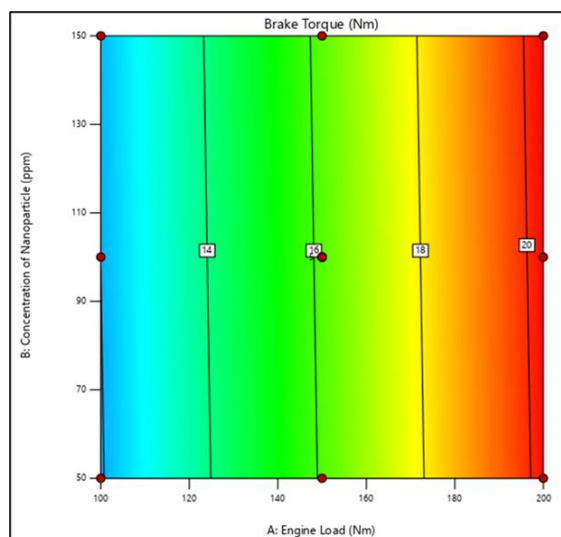


Fig. 2. Interaction effect of nanoparticle concentration and engine speed on brake torque

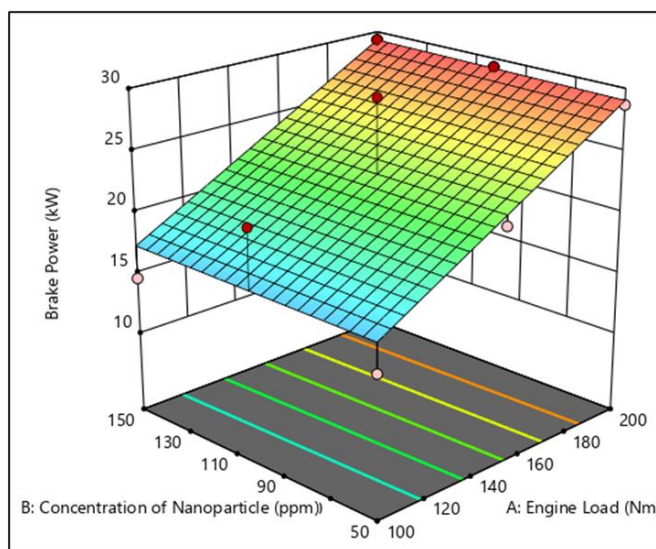
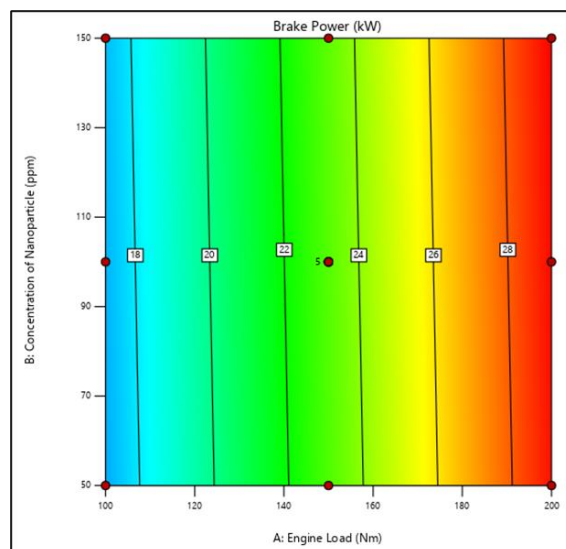


Fig. 3. Interaction effect of nanoparticle concentration and engine speed on brake power

3.3.3 Carbon monoxide (CO) emission

The variation of CO emission with engine speed and nanoparticle concentration in B20 fuel is illustrated in Figure 4. The graph clearly shows that increasing the concentration of nanoparticles in the fuel results in a decrease in CO emissions. This trend suggests that higher nanoparticle concentrations enhance combustion efficiency, leading to more complete fuel combustion. The regression model for estimating CO emissions is presented in Eq. (4).

$$\text{CO Emission} = -0.27 - 0.0183A + 0.015B + 0.005A^2 - 0.055B^2 \quad (4)$$

The combined figure highlights the effectiveness of nanoparticle additives in reducing CO emissions across various engine speeds. Specifically, the presence of SiO₂ nanoparticles in the biodiesel blend significantly lowers the amount of carbon monoxide produced during combustion. This reduction is likely due to the improved catalytic activity of the nanoparticles, which facilitates a more complete oxidation of carbon-based compounds in the fuel. As a result, the emission of partially oxidized products, such as carbon monoxide, is minimized.

3.3.4 Carbon dioxide (CO₂) emission

The interaction effect of engine speed and nanoparticle concentration in biodiesel fuel on CO₂ emission is illustrated in Figure 5. The experimental results indicate that CO₂ content increases with the rise in nanoparticle concentration. This phenomenon can be attributed to the improved combustion efficiency brought about by the addition of nanoparticles. Enhanced combustion results in a more complete oxidation of the fuel, thereby increasing the production of CO₂ as a byproduct.

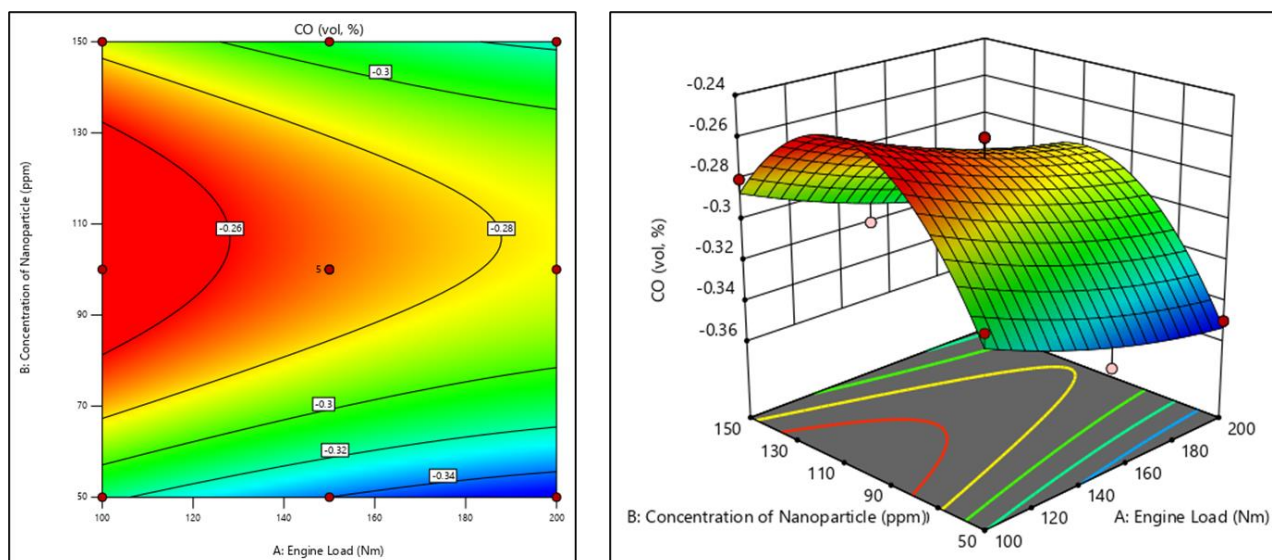


Fig. 4. Interaction effect of nanoparticle concentration and engine speed on CO emission

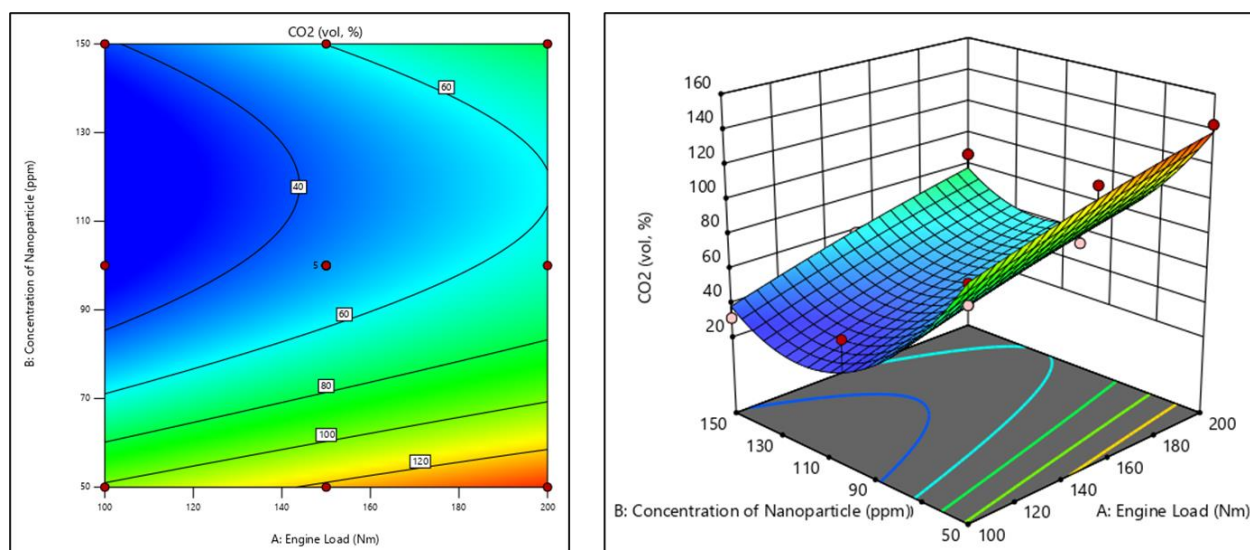


Fig. 5. Interaction effect of nanoparticle concentration and engine speed on CO₂ emission

The amount of CO₂ emission depends on the air-fuel ratio and the concentration of CO emission. As the CO emissions decrease due to more efficient combustion, the conversion of CO-to-CO₂ increases, reflecting the completion of the combustion process. The regression model for estimating CO₂ emissions is presented in Eq. (5).

$$\text{CO}_2 \text{ Emission} = 47.96 + 19.03A - 31.17B + 0.875AB - 1.99A^2 + 43.41B^2 \quad (5)$$

3.3.5 Nitrogen oxides (NO_x) emission

The trend of NO_x emissions with respect to engine speed and nanoparticle concentration in B20 fuel is illustrated in Figure 6. The surface plot indicates that NO_x concentration increases with higher nanoparticle concentrations. This increase can be attributed to the elevated combustion temperatures resulting from the improved combustion efficiency facilitated by the nanoparticles. The regression model for estimating NO_x emissions is presented in Eq. (6).

$$\text{NO}_x \text{ Emission} = 1490.38 - 36.17A + 34.67B + 340.50AB \quad (6)$$

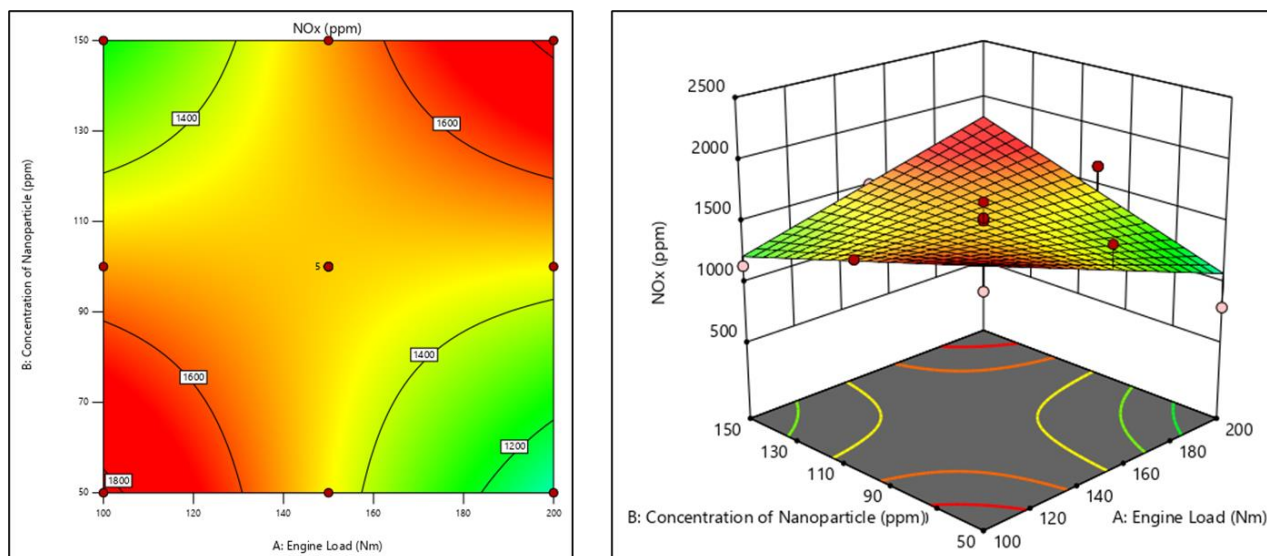


Fig. 6. Interaction effect of nanoparticle concentration and engine speed on NO_x emission

The graph reveals that as the concentration of nanoparticles in the biodiesel blend rises, the NO_x emissions also increase. This trend is primarily due to the higher temperatures achieved during combustion, which promote the formation of nitrogen oxides. While improved combustion efficiency is beneficial for reducing CO and CO₂ emissions, it also necessitates careful management of NO_x emissions to meet environmental regulations. Further research could explore methods to mitigate NO_x formation while maintaining the benefits of enhanced combustion provided by nanoparticle additives.

3.4 RSM-Based Optimization

Optimization using response surface methodology (RSM) revealed significant interactions between engine load, oxide nanoparticle concentration, and emission parameters. The optimization criteria for the response, including their lower and upper limits, importance, and weight, are shown in Table 6. The weights range from 0.1 to 10, with higher weights (>1) indicating greater importance to the objective, while weights less than 1 indicate lesser importance. The relative significance of the parameters varies among them. In this optimization process, more importance is given to CO, CO₂, and NO_x emissions.

Table 6

Optimization criteria of emission and performance parameters

Parameter	Limits		Weight		Importance	Criterion
	lower	upper	lower	upper		
A: Engine load	100	200	1	1	5	In range
B: Concentration of SiO ₂	50	150	1	1	5	In range
Brake torque	10.2	20.4	1	1	5	Maximize
Brake power	14.6	29.3	1	1	5	Maximize
CO	-0.35	-0.26	1	0.1	5	Minimize
CO ₂	31.2	142.9	1	0.1	5	Minimize
NO _x	793	1668	1	0.1	5	Minimize

The optimization process, utilizing a desirability approach, presented five solutions for B20 blended with SiO₂ nanoparticles at different concentrations, as shown in Table 7. Higher desirability solutions, which are closer to the set criteria, are preferred. Among these solutions, Solution 1 optimizes the running condition with a desirability of 0.953, achieved at 200 Nm of engine load and 67.26 ppm of SiO₂ concentration.

Table 7

Solutions of five highest desirability based on optimization criteria

No.	Engine load (Nm)	Concentration of SiO ₂ (ppm)	Brake torque (Nm)	Brake power (kW)	CO (%)	CO ₂ (%)	NO _x (ppm)	Desirability
1	200	67.26	20.26	29.09	0.32	103.44	1208.59	0.953
2	200	51.86	20.24	29.06	0.35	134.41	1092.97	0.905
3	200	51.68	20.24	29.06	0.35	134.82	1091.64	0.933
4	200	72.81	20.27	29.10	0.31	94.31	1250.17	0.929
5	200	79.83	20.28	29.12	0.30	84.28	1302.84	0.908

The optimization study highlights the significant interplay between engine load, SiO₂ nanoparticle concentration, and exhaust emissions. By fine-tuning these parameters, it is possible to achieve optimal engine performance while minimizing harmful emissions. The desirability approach aids in identifying the most favourable operating conditions that balance performance and environmental considerations. Higher engine loads and moderate SiO₂ concentrations (as seen in Solution 1) lead to a desirable balance of high brake torque and power, with reduced CO and NO_x emissions. The increase in CO₂ emissions, although indicative of improved combustion efficiency, requires careful management to ensure compliance with environmental standards.

These findings underscore the potential benefits of integrating SiO₂ nanoparticles into biodiesel blends, promoting cleaner and more efficient marine diesel engine operations. Further studies could explore the long-term effects of nanoparticle additives and investigate alternative nanoparticle materials to further enhance fuel performance and emission control.

4. Conclusions

In conclusion, this study was designed to investigate the combined impacts of blended nanoparticles – palm biodiesel fuel on the engine performance and emission characteristics of a marine diesel engine and to determine the optimization evaluation of various types of nanoparticles blended with palm biodiesel fuels on the performance and emission of a marine diesel engine. The results of the experiments are summarized as follows:

- i. The combined impacts of blended nanoparticles – palm biodiesel fuel have improved biodiesel performance while lowering pollutants from the exhaust.
- ii. The response model produced is found to be significant with p-values of less than 0.05.
- iii. Regression statistics such as goodness of fit (R^2) and goodness of predictions (adjusted R^2) are in good agreement with each other, with the difference between them being less than 0.2, with the exception of NO_x emission, where the difference is greater than 0.2.
- iv. Optimization, with the objective to determine the best desirability, resulted in blended nanoparticles with palm biodiesel fuel at a concentration of 67.26 ppm and an engine load of 200 Nm, achieving a maximum desirability of 95.3%.

These findings demonstrate the potential of nanoparticles to enhance the performance and emission characteristics of biodiesel fuels in marine diesel engines, highlighting their viability as a cleaner and more efficient alternative to conventional fuels. Further research and optimization could continue to improve these outcomes, paving the way for more sustainable marine transportation solutions.

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